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2017-04-04

Investigation of synthetic spider silk crystallinity and alignment via electrothermal, pyroelectric, literature XRD, and tensile techniques

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Original Publication Citation

Munro, T., Putzeys, T., Copeland, C., Xing, C., Lewis, R., Ban, H., Glorieux, C., and Wubbenhorst, M., "Investigation of synthetic spider silk crystallinity and alignment via electrothermal, pyroelectric, literature XRD, and tensile techniques," *Macromolecular Materials and Engineering*, DOI: 10.1002/mame.201600480, 2017.

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Munro, Troy; Putzeys, Tristan; Wubbenhorst, Michael; Glorieux, Christ; Copeland, Cameron G.; Lewis, Randolph V.; Xing, Changhu; and Ban, Heng, "Investigation of synthetic spider silk crystallinity and alignment via electrothermal, pyroelectric, literature XRD, and tensile techniques" (2017). *All Faculty Publications*. 1876.
<https://scholarsarchive.byu.edu/facpub/1876>

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1 DOI: 10.1002/((mame.201600480))

2 **Article type: ((Full Paper))**

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5 **Investigation of synthetic spider silk crystallinity and alignment via electrothermal,**
6 **pyroelectric, literature XRD, and tensile techniques**

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30
31 **Keywords:** spider silk, crystallinity, thermal, pyroelectric, processing

32
33 The processes used to create synthetic spider silk greatly affect the properties of the produced
34 fibers. This paper investigates the effect of process variations during artificial spinning on the
35 thermal and mechanical properties of the produced silk. Property values are also compared to
36 the ones of the natural dragline silk of the *N. clavipes* spider, and to unprocessed (as-spun)
37 synthetic silk. Structural characterization by scanning pyroelectric microscopy is employed to
38 provide insight into the axial orientation of the crystalline regions of the fiber and is supported
39 by XRD data. The results show that stretching and passage through liquid baths induce
40 crystal formation and axial alignment in synthetic fibers, but with different structural
41 organization than natural silks. Furthermore, an increase in thermal diffusivity and elastic
42 modulus is observed with decreasing fiber diameter, trending towards properties of natural
43 fiber. This effect seems to be related to silk fibers being subjected to a radial gradient during
44 production.

45
46 **1. Introduction**

47 In the past decade, a significant research interest has emerged toward spiders and spider silk
48 because of their exceptional mechanical properties^[1,2]. A single orb weaving spider is capable
49 of spinning a multitude of silk types, each emerging from its own particular set of abdominal

1 silk glands, which enable the spider to tailor silk to a single specific task (e.g. web assembly,
2 egg-case construction, prey wrapping, transportation, etc.)^[2-4]. Most silks, in particular
3 dragline silk from the major ampullate gland, possess revolutionary mechanical properties due
4 to their unique combination of high tensile strength with large ductility^[5].

5
6 However, the low yield of harvesting silk from either free or caged spiders limits natural
7 spider silk as a construction material for economic reasons. To overcome this obstacle,
8 numerous processes exist to produce synthetic spider silk, with properties close to the ones of
9 natural spider silk.

10
11 The process to artificially synthesize spider silk into fibers consists of two consecutive
12 pathways: the synthesis of the feedstock (the unspun silk dope in spiders) and mimicking the
13 mechanical spinning conditions (the funnel, valve, tapering duct, and spigot)^[6]. For protein
14 production, the synthetic protein host can limit the size of the repeated amino acid sequence,
15 limiting the size of the expressed protein^[7], which can affect the fiber spinning and the fiber's
16 properties. In 2000, the Canadian biotechnology company Nexia successfully produced spider
17 silk protein in transgenic goats that carried the gene for it, where the milk produced by the
18 goats contained significant quantities of the two proteins present in the natural silk^[8,9]. The
19 Lewis Spider Silk Lab has produced fibers from recombinant spider silk protein from
20 transgenic goats^[10-13].

21
22 Mimicking the natural spinning process of the spider is an ongoing challenge for spider silk
23 production. The protein dope (composed of both MaSp1 and MaSp2 proteins^[14,15]) inside the
24 spider is water-soluble, but until recently^l, recombinant proteins have only been solubilized in
25 a chaotropic agent, HFIP (hexafluoroisopropanol), at concentrations lower than the ones
26 found naturally in the spider. Recent work has successfully spun recombinant proteins from
27 aqueous solutions rather than HFIP^[9,16-18] where significant fluctuations in the mechanical
28 properties were observed due to the non-optimized process for fiber and film production. The
29 spinning of the protein dope into a usable fiber must then attempt to mimic the processes in
30 the spider ducts where water is removed and the proteins folds into a water-insoluble fiber^[6].
31 Microfluidic channels (where ionic concentrations and pH can be carefully controlled) have
32 been able to produce small quantities of synthetic silk^[18,19], but this process is difficult to
33 scale-up for the commercial production of spider silk. A continuous extrusion machine has
34 been used to successfully produce large quantities (>500m per dope), with the fiber passing
35 through baths of aqueous solutions that aid HFIP removal and protein secondary structure
36 formation^[10]. The synthetic silks generated by this machine from recombinant protein
37 produced by transgenic goats and their comparison to natural dragline silk are the focus of the
38 current study.

39
40 In a previous study, it has been noted that the process pathway of spinning the synthetic silk
41 will have great influence on the final material properties^[10]. Some of these properties of the
42 natural and synthetic spider silks have been reported in literature (mechanical^[11,20] and
43 thermal^[21,22]), but the pyroelectric response of silk is lacking in the literature. To this end, the
44 thermal diffusivity, thermal conductivity, and local pyroelectric response have been measured
45 in the current study for different post-extrusion processes of synthetic spider silk. This is the
46 first time the mechanical, thermal, and pyroelectric behavior of both natural and synthetic
47 dragline silk have been investigated in the literature and compared.

48
49 This study focuses on the effect of processing conditions on the thermal and mechanical
50 properties of synthetic silk, created from spidroin proteins from transgenic goat milk by
51 means of a spinning process that makes use of a modified plastic extruder. These properties

1 are correlated to each other, to their pyroelectric response, and to the final diameter of the
2 fiber. Literature values and diagrams of the crystalline alignment from XRD are also
3 compared to thermal diffusivity and fiber diameter. These observations between the different
4 material characteristics provide insight into processing aspects that improve the synthetic
5 silk's properties and a potential mechanism is proposed to explain why synthetic silks have
6 lower thermal and mechanical properties than natural silks.

9 **2. Experimental Description**

10 This section covers the formation and preparation of the silk samples as well as the material
11 characterization setups.

13 **2.1 *Nephila clavipes* Silk Collection**

14 Silk was collected from adult *Nephila clavipes* spiders, which originated from the state of
15 Florida, US. Silk was collected using the method described by Xu et al.^[14] Briefly, spiders
16 were anesthetized by exposing them to CO₂, allowing them to be restrained on the top of a
17 Petri dish. With a dissecting microscope, the spinnerets for dragline silk were located and then,
18 using tweezers, the silk was teased out of the major ampullate gland. The silk was attached to
19 a rotating spool and approximately 100 meters of silk was gathered, at a silking rate of about
20 2 m/min. To prevent dehydration, the spiders were misted during the spooling process.

22 **2.2 Synthetic Silk Production**

23 Recombinant spider silk protein was produced using the method described by Tucker et. al^[9].
24 Briefly, spider silk protein is produced by transgenic goats. Goats produce either the MaSp1
25 protein or MaSp2 protein when they lactate, and the proteins are found in their milk. Each
26 protein is approximately 65kDa long and contains the non-repetitive C-terminal and the
27 repetitive region of the protein. Milk was defatted and then combined with 0.1M L-arginine-
28 HCL (Spectrum Chemical MFG. Corp., Gardena, CA) in a 1:1 ratio. The pH was adjusted to 9,
29 the milk was mixed for 30 minutes, and then loaded on a custom system of tangential flow
30 filters. For 24 hours, the milk was filtered and the concentrated whey was collected.
31 Ammonium sulfate was added to the whey at a concentration of 1.2M and then mixed for 24
32 hours to salt out the protein. The protein was then serially washed and centrifuged with
33 distilled water until the electrical conductivity of the runoff was less than 20 μS. The protein
34 was then lyophilized.

36 Spider silk fibers were produced using the recombinant spider silk protein according to the
37 method described by Copeland et. al^[10]. Briefly, a spin dope was prepared by placing MaSp1
38 and MaSp2 proteins in a 4mL vial with a Teflon lid (Waters Associates, Milford MA). The
39 two proteins were mixed in the same ratio as has been observed in the native *Nephila clavipes*
40 spider^[23], i.e. a 4:1 ratio of MaSp1 and MaSp2. HFIP (Oakwood Chemical, West Columbia,
41 SC) and 88+% formic acid (Alfa Aesar, Ward Hill, MA) were added to the vial in a ratio of
42 4:1 (v/v). The final concentration of the protein in solution was 25% (w/v). The solution was
43 mixed by slowly rotating for 48 hours until all the protein was dissolved and the spin dope
44 was observed to be homogenous. Impurities were removed by centrifuging the vials at 4180
45 rcf for 24 hours and pouring the spin dope into a new vial. The spin dope was loaded into a
46 1mL Hamilton syringe (Hamilton Company, Reno, NV) with 10cm of PEEK tubing (internal
47 diameter 0.005") (SUPELCO, Bellefonte, PA) attached for tubing. The syringe was placed in
48 a modified DACA Spinline (DACA Instruments, Santa Barbara, CA) and extruded at a rate of
49 0.7mm per minute into a coagulation bath comprised of 100% IPA (Pharmo-Products Inc.,
50 Brookfield CT). As-spun (or extruded) fibers were collected at this stage of the process.

1 Single stretched fibers were collected after being run through two sets of Godets with an
 2 alcohol/water stretch bath between them. Double stretched fibers went through the same set of
 3 Godets as the first bath but were then stretched again in a distilled water bath. A schematic of
 4 the processing equipment is also provided in **Figure 2** and by Copeland et. al^[10].

6 **2.3 Thermal Diffusion/Conductivity Measurement Setup**

7 The thermal diffusivity of the spider silk fibers was measured by an improved transient
 8 electrothermal technique (TET)^[24]. The details of the technique can be found in Ref^[25].
 9 Basically, fibers were suspended between two constant temperature heat sinks, coating the
 10 fibers in several nanometers of gold to make them electrically conductive, placing the fibers
 11 in a high vacuum to eliminate convective effects, passing a constant current to the metal film,
 12 and measuring the voltage drop across the film (which relates directly to the resistance change
 13 of the film) as the fiber temperature increases, **Figure 1**. The transient behavior relates to the
 14 thermal diffusivity of the fiber (Equation 1, which is a reduced model that does not consider
 15 radiation heat losses) and the steady state behavior relates to the thermal conductivity, when a
 16 temperature-resistance correlation is measured (Equation 2, which is a reduced model that
 17 also does not consider radiation heat transfer). Full models of these property relationships that
 18 include additional modes of heat transfer behavior (including radiation, convection, and non-
 19 constant Joule heating) are found in Ref^[24], and can provide additional accuracy to the
 20 measurement when the sample geometry is known in detail.

$$22 \quad \frac{\overline{\Delta T}}{\Delta T_s} = \frac{\Delta V}{\Delta V_s} = 1 - \frac{96}{\pi^4} \sum_{m=1}^{\infty} \frac{e^{-(2m-1)^2 \pi^2 \alpha t / L^2}}{(2m-1)^4} \quad (1)$$

$$23 \quad k = \frac{I^2 R_0 R' L}{3\pi D^2 (R_s - R_0)} \quad (2)$$

24 Because of the non-uniform geometries of processed synthetic spider silks (seen in the SEM
 25 images of **Figure 3**), determination of their thermal conductivity was not possible. To that end,
 26 the best approach is to determine the diffusivity of multiple fibers that underwent the same
 27 production process, assume that they have the same radiation characteristics, and curve-fit the
 28 property values as a function of the square of the length to determine a “zero-length” property.
 29 This “zero-length” value is where radiation heat loss would not over-predict the property
 30 measurement^[21] and provides an accurate thermal diffusivity value.

33 **2.4 Pyroelectric Setup**

34 A scanning pyroelectric microscope (SPEM) measurement results in a pyroelectric response
 35 distribution map that can be directly correlated to the local spontaneous polarization
 36 distribution. SPEM is a proven technique^[26] for the determination of a polarization
 37 distribution map with both lateral and depth resolution by scanning the laser beam over the
 38 sample surface and modulating the laser output at different frequencies. This method has been
 39 used successfully for pyroelectric crystals with dimensions on the order of tens to hundreds of
 40 micrometers.

41
 42 Briefly, SPEM involves a modulated laser beam that induces a local harmonic change in
 43 temperature. If the illuminated region is pyroelectric, it generates a small electric current,
 44 which can then be measured by two parallel plate electrodes. The pyroelectric current vector
 45 is proportional to the local electrical polarization vector, and by scanning the laser beam over

1 different regions of the sample, the polarization distribution map can be obtained. The power
2 modulation of the laser output is typically on the order of 10 to 100 mW peak-to-peak power,
3 with laser beam spot sizes ranging from 20 to 1 micrometers in diameter (depending on the
4 optics and laser source used). The pyroelectric current that is generated is on the order of
5 femtoamperes (10^{-15} A). To this end, a series of noise-reducing techniques have been
6 employed and are explained in more depth in Ref^[26].

7
8 The local macroscopic polarization is dependent on both the local symmetry and the dipole
9 moment of the oriented molecules, which in this case is spidroin crystallites. Because of this,
10 the SPEM image is also indicative of changes in macroscopic orientation in the same sample.
11 The pyroelectric response can then be used to compare the degree of macroscopic orientation
12 between different samples if they are composed of the same material, which is the case with
13 the spider silks investigated in this study. Having the same ratio of MaSp1 and MaSp2
14 proteins (80:20) in all synthetic fibers, the differences in the silk are merely due to the process
15 they went through to be produced.

16 17 **2.5 SEM Setup**

18 SEM images were taken with a FEI Quanta FEG 650 microscope, at energies of 15 and 30 kV,
19 after being placed on carbon tape and coated with 10 nm of gold. The fibers imaged were
20 taken from the same strand of silk as the fibers used for thermal, pyroelectric, and mechanical
21 testing. Three images of each fiber were taken and the diameter was measured at two
22 locations on the fiber in each image (**Figure 3**).

23 24 **2.6 XRD**

25 X-ray fiber diffraction was performed on the BioCars 14bm-C beamline on samples measured
26 at the Advanced Photon Source located at Argonne National Laboratory, Argonne IL, USA.
27 Fibers were mounted and placed at a distance of 300mm from the detector. Stretched fibers
28 were placed with the stretched axis normal to the beam line. For a single image, data
29 collection times were 60 seconds and ten images were taken for each sample. Background
30 images were taken right after each sample was completed with identical parameters. Images
31 were then processed using Fit2D software. XRD results have been presented previously in
32 literature^[10], and the improvement on crystallinity and axial alignment of fibers observed by
33 XRD during processing of the fibers agrees well with the results from the current study. In the
34 following, XRD diffraction patterns will be presented with the thermal diffusivity and fiber
35 diameter results.

36 37 **3. Results**

38 **3.1. Natural Dragline Silk from *Nephila clavipes***

39 Natural spider silk has received significant consideration in the literature, because of its
40 favorable materials properties. Of particular interest is the dragline silk from the *Nephila*
41 *clavipes*, with high strength, elongation, and toughness for a polymer and low density
42 material^[14]. These values are typically in the range of 0.7-1.4 GPa ^[20,27,28] for ultimate tensile
43 strength, 6-35 % for elongation^[20,29-31], and 100-400 kJ kg⁻¹ for toughness or energy-to-
44 break^[27,31].

45
46 In the literature, initial studies on the thermal properties of dragline silk reported an
47 exceptionally high thermal conductivity, comparable to copper, which improved upon
48 stretching^[32]. Originally, these high values were attributed to the crystalline β -sheets that
49 exist in the natural dragline silk (as shown by XRD^[33]). However, further investigation of the

1 thermal diffusivity^[21,34] and thermal conductivity^[21] of the natural dragline silk demonstrated
2 that the initial results were erroneous, due to neglecting the radiation heat transfer
3 contribution, to insufficient vacuum to eliminate convection, and to length dependence of the
4 thermal property measured. The results presented in the current study take these additional
5 considerations into account, thus yielding the additional accuracy needed to compare the
6 natural to the synthetic spider silk. The value found for the thermal conductivity of dragline
7 silk is $1.2 \text{ W m}^{-1} \text{ K}^{-1}$ and for the thermal diffusivity $6 \times 10^{-7} \text{ m}^2 \text{ s}^{-1}$, with 12% uncertainty^[21].
8 These values are considerably more reasonable for a semi-crystalline, protein-based polymer,
9 such as human hair^[35] or a different species of spider^[34]. Additionally, molecular dynamics
10 simulations have shown that the β -sheets (that were the original explanation for the high
11 conductivity of the dragline silk) have a thermal conductivity of only 2-4 $\text{W m}^{-1} \text{ K}^{-1}$,
12 depending on the number of strands in the sheet^[36].

13
14 The polarization distribution of natural spider silk, measured using SPEM, displays a
15 pyroelectric response in the radial orientation (**Figure 4**). This observation implies a
16 macroscopic orientation of the spidroin crystallites, probably caused by the extrusion via the
17 spinneret. This correlates with XRD and NMR results looking at the structure of natural
18 spider silk^[37-39]. It is possible that the pyroelectric and (inferred via symmetry properties)
19 piezoelectric properties potentially serve a physiological function, serving as temperature
20 and/or pressure sensors (as hypothesized for the chitin wings of certain insects^[40]).

21 22 **3.2. Extruded (As-Spun) Synthetic Spider Silk**

23 The as-spun synthetic spider silk provides a baseline to compare the effect of processing on
24 synthetic spider silks, because it contains the necessary protein content, but does not have the
25 same microstructure as other silks. This is demonstrated by the severe brittleness of the fibers
26 as they break easily when handled. Furthermore, XRD results in the literature have shown that
27 the as-spun fiber has no appreciable crystalline content^[10,11].

28
29 The thermal properties of the as-spun synthetic spider silk were measured by the improved
30 TET technique. Because of their uniform surface geometry, the thermal conductivity and
31 thermal diffusivity can both be determined. The magnitudes of these values are $0.25 \text{ W m}^{-1} \text{ K}^{-1}$
32 for the thermal conductivity and $1.68 \times 10^{-7} \text{ m}^2 \text{ s}^{-1}$ for the thermal diffusivity, similar to
33 synthetic films measured in Ref.^[41]. This is almost 6 times lower than the thermal transport
34 values measured for natural spider silk. These significantly lower properties are also
35 observed in the mechanical properties (32.5 MPa for ultimate tensile strength, 1% for
36 extensibility, and 0.18 kJ kg^{-1} for toughness), and this decrease is attributed to the lack of
37 crystallinity that exists based on XRD investigation of the silks^[11]. The XRD diffraction
38 pattern indicates weak alignment of the spidroin protein crystallites which is in line with the
39 pyroelectric measurement (a direct indication of local macroscopic alignment) and the low
40 thermal diffusivity and conductivity.

41
42 The pyroelectric SPEM response map of extruded synthetic silk (**Figure 5**, top) primarily
43 displays an axial polarization component, whereas natural silk has a dominating radial
44 component. Unlike the natural silk, the as-spun synthetic silk displays a coaxial polarization,
45 seen primarily with the low frequency image that represents structure deeper in the fiber
46 (Figure 5, top right). The axial alignment arises from the axial extrusion process, forcing the
47 synthetic spidroin crystallites in a macroscopic axial orientation. The coaxial behavior could
48 be due to a number of effects, the most likely being the existence of a thermal gradient in the
49 thick synthetic silk fiber during the sol-gel transition. A high frequency pyroelectric scan
50 which represents surface behavior reveals several domains in the axial orientation (Figure 5,

1 top left), corresponding to the rough texture seen in the SEM images. This could well be the
2 result of a polar self-assembly process during the extrusion^[42].

3
4 Further stretching and processing of the extruded silk fiber could result in greater macroscopic
5 alignment of the crystallites, yielding thermal and mechanical properties closer to the ones of
6 natural silk.

7 8 **3.3. Processed Synthetic Silk**

9 The thermal diffusivity values of several synthetic spider silks with different processes have
10 been measured. The non-uniformities of the synthetic spider silks' geometry would add
11 significant errors to the thermal conductivity measurement^[21] because of the need for an
12 accurate volumetric heating in the model, so the thermal conductivity is not reported.
13 However, the sensitivity of the thermal diffusivity (proportional to the thermal conductivity
14 by the expression $\alpha=k/\rho c_p$) to processing variations should be sufficient as a metric because
15 the diffusivity measurement is not affected by sample volume. To that end, eight different
16 processed silks have been measured, based on different processing variations of the spinning
17 apparatus shown in Figure 2. These variations fall into the following categories: (1) %
18 volume of solution contents in solution bath B – IPA/H₂O/MeOH, (2) use of pure water bath
19 D for dipping or stretching, and (3) extent of stretching in the liquid baths that the fiber passes
20 through – 2x, 3x. Their properties and pyroelectric response are best compared to each other
21 and to the natural spider silk they are meant to mimic in the next section.

22 23 **3.4. Comparison between Natural and (Processed) Synthetic Silk**

24 When comparing extruded synthetic silk to further processed silk, a favorable increase in the
25 investigated material properties is observed. Further processing of the extruded silk results in
26 increased thermal diffusivity, predicted thermal conductivity, pyroelectric response, and
27 macroscopic crystalline β -sheet orientation.

28
29 **Figure 6** and **Figure 7** show the relationship between the thermal diffusivity of each silk
30 compared to its mechanical properties and pyroelectric response. There is a noticeable
31 correlation: an improvement in one property is mirrored in an improvement of the other
32 properties. This is indicative of improvements in the organization of the silk's microstructure,
33 as crystalline β -sheets are formed upon passing of the fiber through the solution baths (shown
34 by XRD^[10] and **Figure 8**) and increased axial alignment of the dipoles due to the stretching
35 (shown by SPEM, Figure 5, bottom).

36
37 It is interesting to note that the increase in material properties has an inverse correlation to the
38 silk's diameter, i.e. a decrease in diameter corresponds to an increase in thermal diffusivity or
39 pyroelectric response (Figure 8). It is likely that the repeated stretching and solution-dipping
40 (which results in a smaller diameter) also reduces the radial gradient in material properties, as
41 evidenced by the pyroelectric data. This produces a fiber that is more uniform in both the
42 axial and radial directions and better resembles the crystallites' orientation in native silk. As
43 stretching causes elongation in one direction, conservation of mass and density dictates that
44 the other dimensions should shrink. In addition, this stretching causes flow alignment of the
45 crystallites, increasing macroscopic orientation. However, there is a limit to the amount of
46 stretching and diameter reduction that can occur without failure of the fiber. One potential
47 option for smaller diameter fiber would be to use a smaller diameter extrusion outlet.
48 However, with smaller diameter extrusion the chance for breaks in the fiber during production
49 are higher for even the smallest non-homogeneity in the spin dope. These potential

1 inhomogeneities could be overcome with an increase of the protein size to more closely
2 mimic natural spider silk.

4 **4. Conclusions and Outlook**

5 The measurement of material strength, thermal diffusivity and local pyroelectric response for
6 synthetic silk created by varying processes clearly indicates a positive correlation between
7 these material properties and a decrease in the fiber's diameter.

8
9 Further processing and stretching of the extruded silk reduces its diameter, introducing an
10 axial flow alignment of the spiderin crystallites. When the β -sheet spiderin crystallites enjoy a
11 high degree of macroscopic orientation, they allow for a better transmission of heat
12 conduction and increased tensile strength. The high degree of orientation is also responsible
13 for a high spontaneous polarization and associated pyroelectric response to small thermal
14 perturbations.

15
16 These findings (particularly the polarization findings by SPEM and potential radial gradient
17 during fiber processing) imply that for the large scale production of synthetic spider silk that
18 more closely mimics the behavior of the natural dragline silk, care must be taken to reduce the
19 radial gradient of the fiber during processing. This work has demonstrated that this can be
20 accomplished by stretching, but other mechanisms to decrease the fiber size could potentially
21 improve the fibers' properties. Furthermore, control of the diameter could also provide the
22 ability to tune the properties of the fiber for future applications.

24 **Acknowledgements**

25 The authors would like to acknowledge the support from KU Leuven research project
26 OT/11/064 (Investigation of exotic thermal and elastic behavior of soft matter and functional
27 thin layers by means of advanced experimental techniques), USTAR, the National Science
28 Foundation, and the Department of Energy.

30
31 We acknowledge the support from the Microscopy Core Facility at Utah State University for
32 the SEM work.

33 T. Munro, C. Copeland, and T. Putzeys contributed equally to this work.

36 Received: ((will be filled in by the editorial staff))

37 Revised: ((will be filled in by the editorial staff))

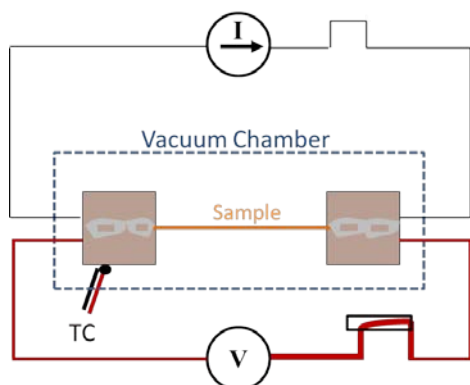
38 Published online: ((will be filled in by the editorial staff))

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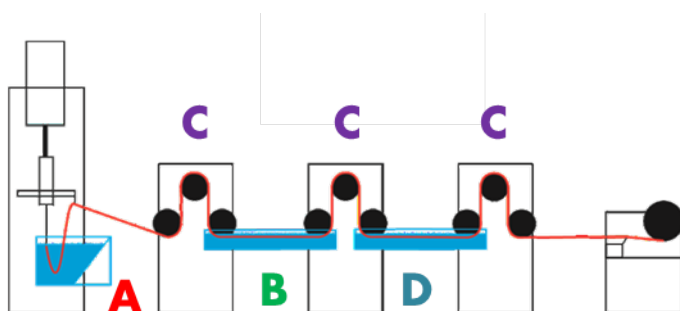
References

- [1] I. Agnarsson, M. Kuntner, T. A. Blackledge, *PloS One* **2010**, *5*, e11234.
- [2] R. V. Lewis, *Chem. Rev.* **2006**, *106*, 3762.
- [3] J. M. Gosline, M. E. DeMont, M. W. Denny, *Endeavour* **1986**, *10*, 37.
- [4] J. M. Gosline, P. A. Guerette, C. S. Orllepp, K. N. Savage, *J. Exp. Biol.* **1999**, *202*, 3295.
- [5] C. Boutry, M. Řezáč, T. A. Blackledge, *PloS One* **2011**, *6*, e22467.
- [6] J. G. Hardy, L. M. Römer, T. R. Scheibel, *Polymer* **2008**, *49*, 4309.
- [7] X.-X. Xia, Z.-G. Qian, C. S. Ki, Y. H. Park, D. L. Kaplan, S. Y. Lee, *Proc. Natl. Acad. Sci.* **2010**, *107*, 14059.
- [8] K. Costas N, T. Jeffrey D, K. Anthoula, Production of Biofilaments in Transgenic Animals, US Patent 7,157,615 **2001**.
- [9] C. L. Tucker, J. A. Jones, H. N. Bringham, C. G. Copeland, J. B. Addison, W. S. Weber, Q. Mou, J. L. Yarger, R. V. Lewis, *Biomacromolecules* **2014**, *15*, 3158.
- [10] C. G. Copeland, B. E. Bell, C. D. Christensen, R. V. Lewis, *ACS Biomater. Sci. Eng.* **2015**.
- [11] F. Teulé, B. Addison, A. R. Cooper, J. Ayon, R. W. Henning, C. J. Benmore, G. P. Holland, J. L. Yarger, R. V. Lewis, *Biopolymers* **2012**, *97*, 418.
- [12] B. An, M. B. Hinman, G. P. Holland, J. L. Yarger, R. V. Lewis, *Biomacromolecules* **2011**, *12*, 2375.
- [13] A. E. Albertson, F. Teulé, W. Weber, J. L. Yarger, R. V. Lewis, *J. Mech. Behav. Biomed. Mater.* **2014**, *29*, 225.
- [14] M. Xu, R. V. Lewis, *Proc. Natl. Acad. Sci.* **1990**, *87*, 7120.
- [15] M. B. Hinman, R. V. Lewis, *J. Biol. Chem.* **1992**, *267*, 19320.
- [16] J. A. Jones, T. I. Harris, C. L. Tucker, K. R. Berg, S. Y. Christy, B. A. Day, D. A. Gaztambide, N. J. Needham, A. L. Ruben, P. F. Oliveira, others, *Biomacromolecules* **2015**, *16*, 1418.
- [17] Q. Peng, Y. Zhang, L. Lu, H. Shao, K. Qin, X. Hu, X. Xia, *Sci. Rep.* **2016**, *6*, 36473.
- [18] A. Heidebrecht, L. Eisoldt, J. Diehl, A. Schmidt, M. Geffers, G. Lang, T. Scheibel, *Adv. Mater.* **2015**, *27*, 2189.
- [19] S. Rammensee, U. Slotta, T. Scheibel, A. Bausch, *Proc. Natl. Acad. Sci.* **2008**, *105*, 6590.
- [20] P. M. Cunniff, S. A. Fossey, M. A. Auerbach, J. W. Song, D. L. Kaplan, W. W. Adams, R. K. Eby, D. Mahoney, D. L. Vezie, *Polym. Adv. Technol.* **1994**, *5*, 401.
- [21] C. Xing, T. Munro, B. White, H. Ban, C. Copeland, R. Lewis, *Polymer* **2014**, *55*, 4226.
- [22] W. Huang, S. Krishnaji, X. Hu, D. Kaplan, P. Cebe, *Macromolecules* **2011**, *44*, 5299.
- [23] A. E. Brooks, H. B. Steinkraus, S. R. Nelson, R. V. Lewis, *Biomacromolecules* **2005**, *6*, 3095.
- [24] C. Xing, T. Munro, C. Jensen, H. Ban, *Meas. Sci. Technol.* **2013**, *24*, 105603.
- [25] C. Xing, T. Munro, C. Jensen, B. White, H. Ban, C. G. Copeland, R. V. Lewis, *Meas. Sci. Technol.* **2014**, *25*, 115604.
- [26] T. Putzeys, M. Wübbenhorst, *Dielectr. Electr. Insul. IEEE Trans. On* **2012**, *19*, 1186.
- [27] S. Mukhopadhyay, J. Sakthivel, *J. Ind. Text.* **2005**, *35*, 91.
- [28] R. S. Rengasamy, M. Jassal, C. Rameshkumar, *AUTEX Res J* **2005**, *5*, 30.
- [29] D. O'Sullivan, *Chem. Eng. News* **1988**, *66*, 24.
- [30] Y. Yang, X. Chen, Z. Shao, P. Zhou, D. Porter, D. P. Knight, F. Vollrath, *Adv. Mater.* **2005**, *17*, 84.
- [31] J. M. Gosline, M. E. DeMont, M. W. Denny, *Endeavour* **1986**, *10*, 37.
- [32] X. Huang, G. Liu, X. Wang, *Adv. Mater.* **2012**, *24*, 1482.

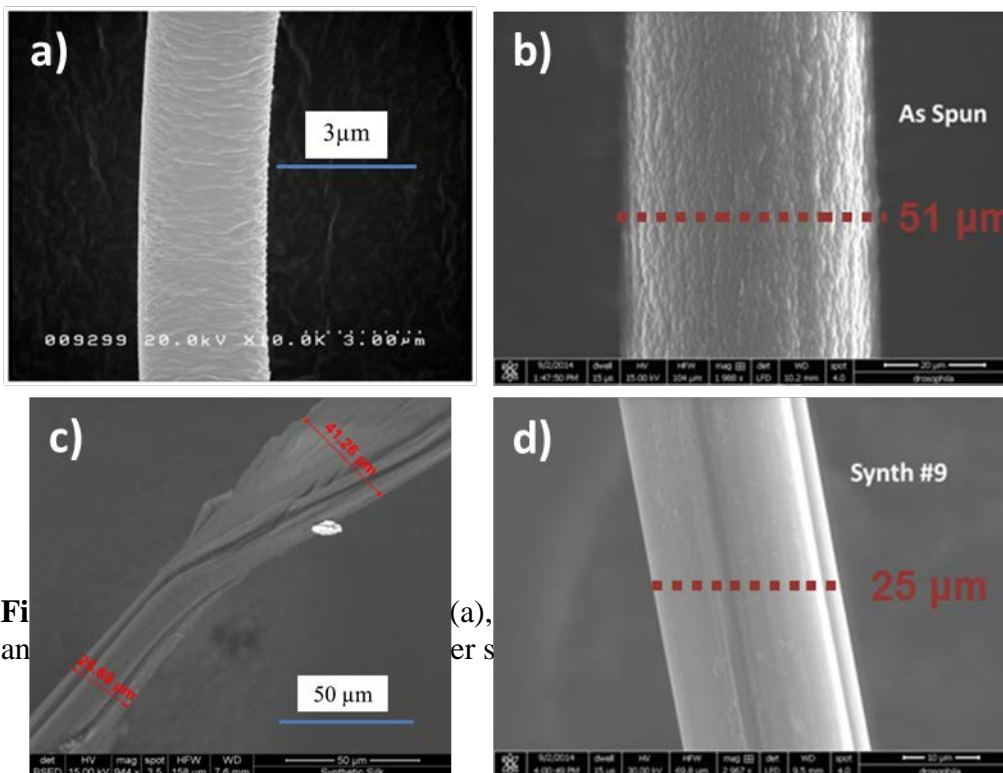
- 1 [33] A. Bram, C. Bränden, C. Craig, I. Snigireva, C. Riekkel, *J. Appl. Crystallogr.* **1997**, *30*,
2 390.
- 3 [34] R. Fuente, A. Mendioroz, A. Salazar, *Mater. Lett.* **2014**, *114*, 1.
- 4 [35] A. Salazar, A. Mendioroz, R. Celorrio, others, *J. Appl. Phys.* **2010**, *107*, 043508.
- 5 [36] L. Zhang, T. Chen, H. Ban, L. Liu, *Nanoscale* **2014**, *6*, 7786.
- 6 [37] S. Sampath, T. Isdebski, J. E. Jenkins, J. V. Ayon, R. W. Henning, J. P. R. O. Orgel, O.
7 Antipoa, J. L. Yarger, *Soft Matter* **2012**, *8*, 6713.
- 8 [38] G. P. Holland, M. S. Creager, J. E. Jenkins, R. V. Lewis, J. L. Yarger, *J. Am. Chem.*
9 *Soc.* **2008**, *130*, 9871.
- 10 [39] M. S. Creager, J. E. Jenkins, L. A. Thagard-Yeamon, A. E. Brooks, J. A. Jones, R. V.
11 Lewis, G. P. Holland, J. L. Yarger, *Biomacromolecules* **2010**, *11*, 2039.
- 12 [40] T. Putzeys, M. Wubbenhorst, *Dielectr. Electr. Insul. IEEE Trans. On* **2015**, *22*, 1394.
- 13 [41] S. Xu, Z. Xu, J. Starrett, C. Hayashi, X. Wang, *Polymer* **2014**, *55*, 1845.
- 14 [42] J. Hulliger, *Chem. - Eur. J.* **2002**, *8*, 4578.
- 15 [43] S. Asha, Y. Sangappa, S. Ganesh, *J. Spectrosc.* **2015**, 2015.
- 16
17



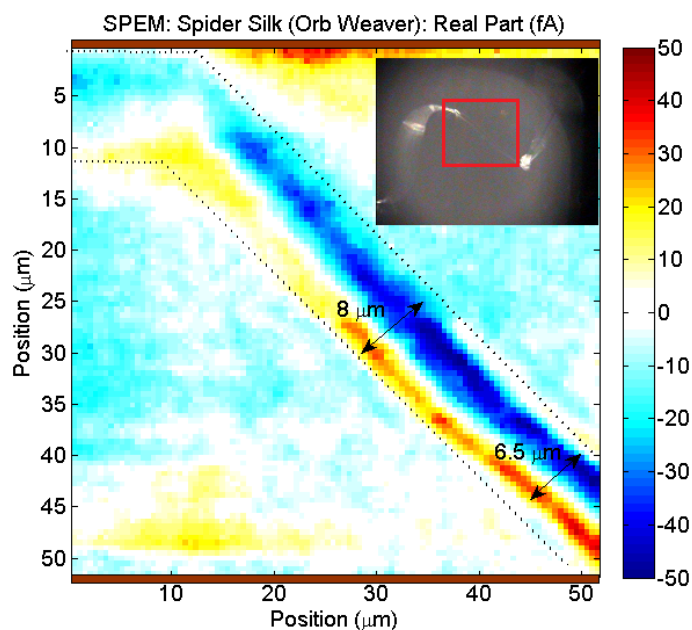
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2 **Figure 1.** Schematic of improved TET method showing step current input and voltage
3 response of sample.
4



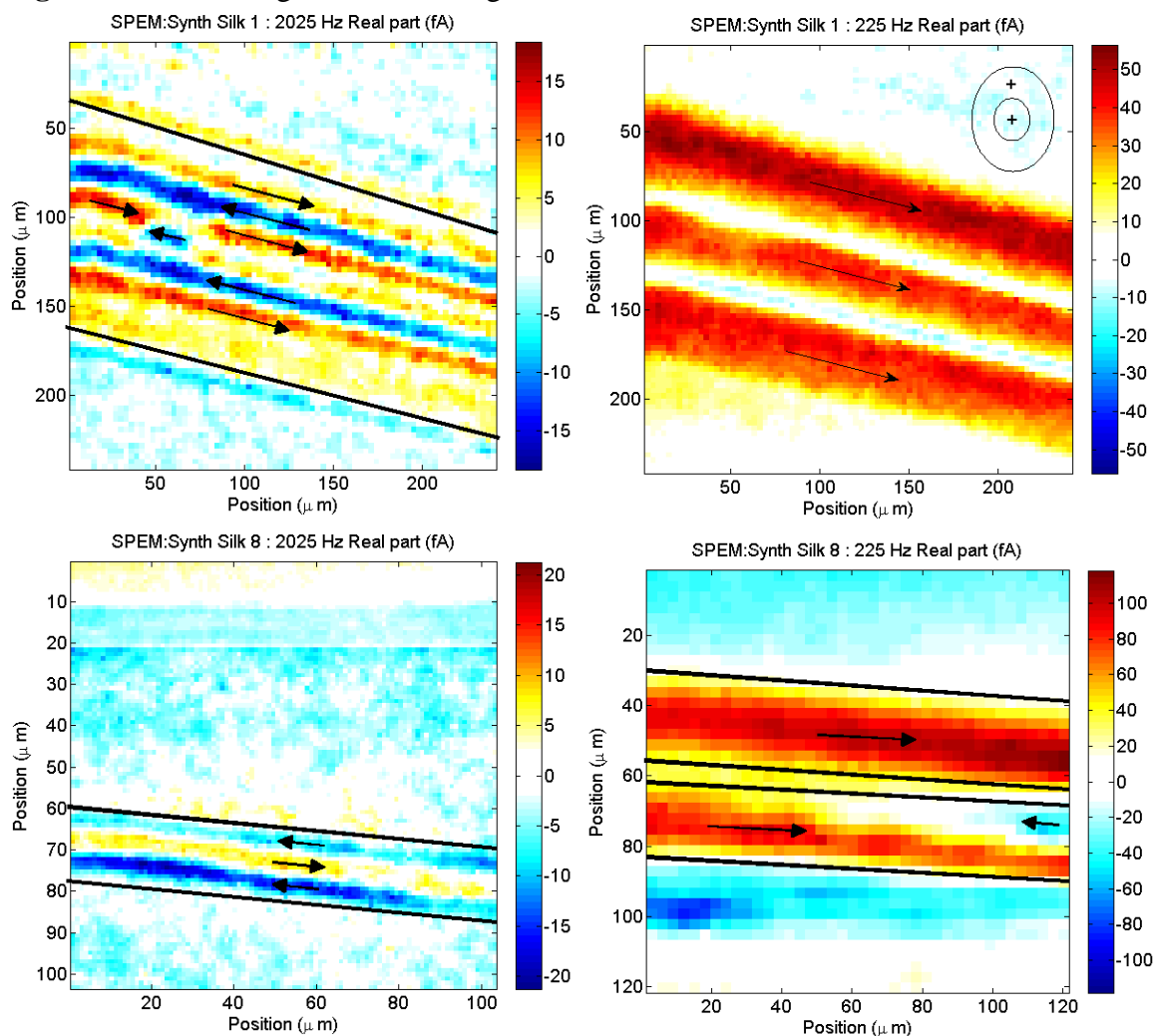
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6 **Figure 2.** Synthetic spider silk spinning apparatus, (A) is coagulation bath, (B) is initial
7 solution bath (either IPA/H₂O or MeOH/H₂O, with details provided in the text), (C) are
8 godets for stretch rate control, and (D) is pure DI water bath.
9



10 **Fi**
11 **an** (a),
12 **er s** ynthetic (c),
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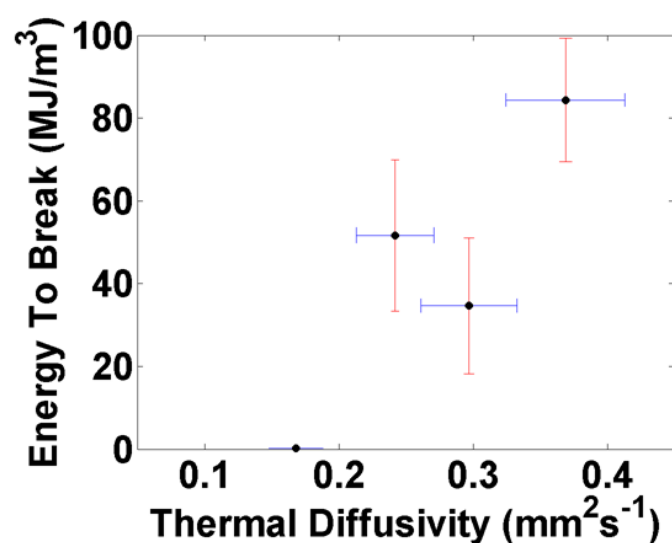
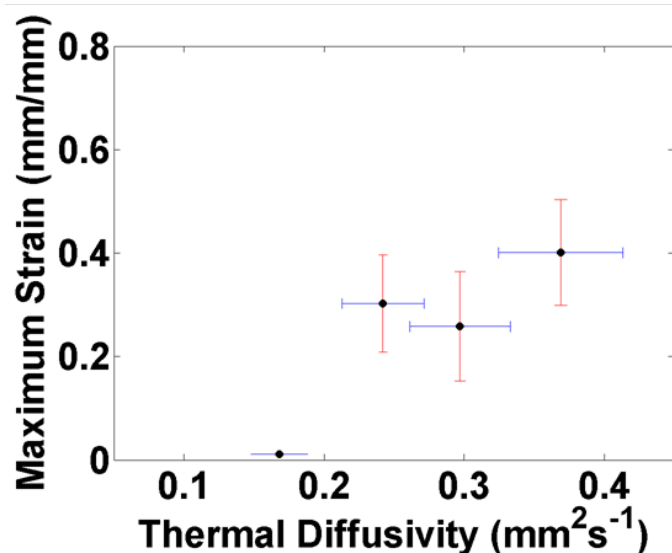
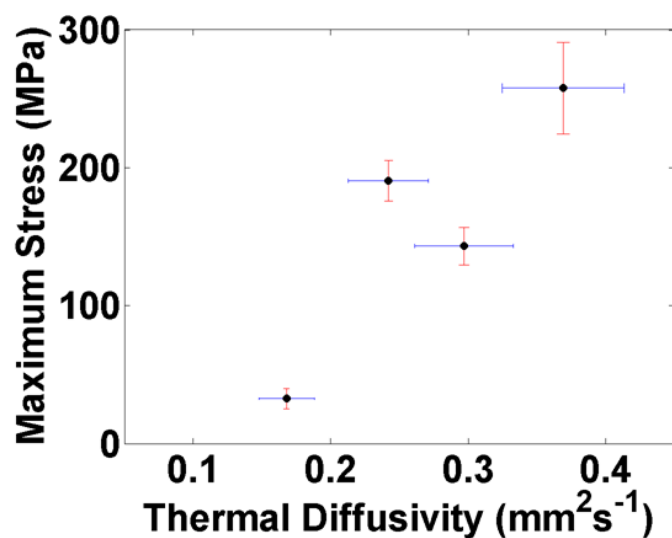


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2 **Figure 4.** SPEM image of natural dragline silk.

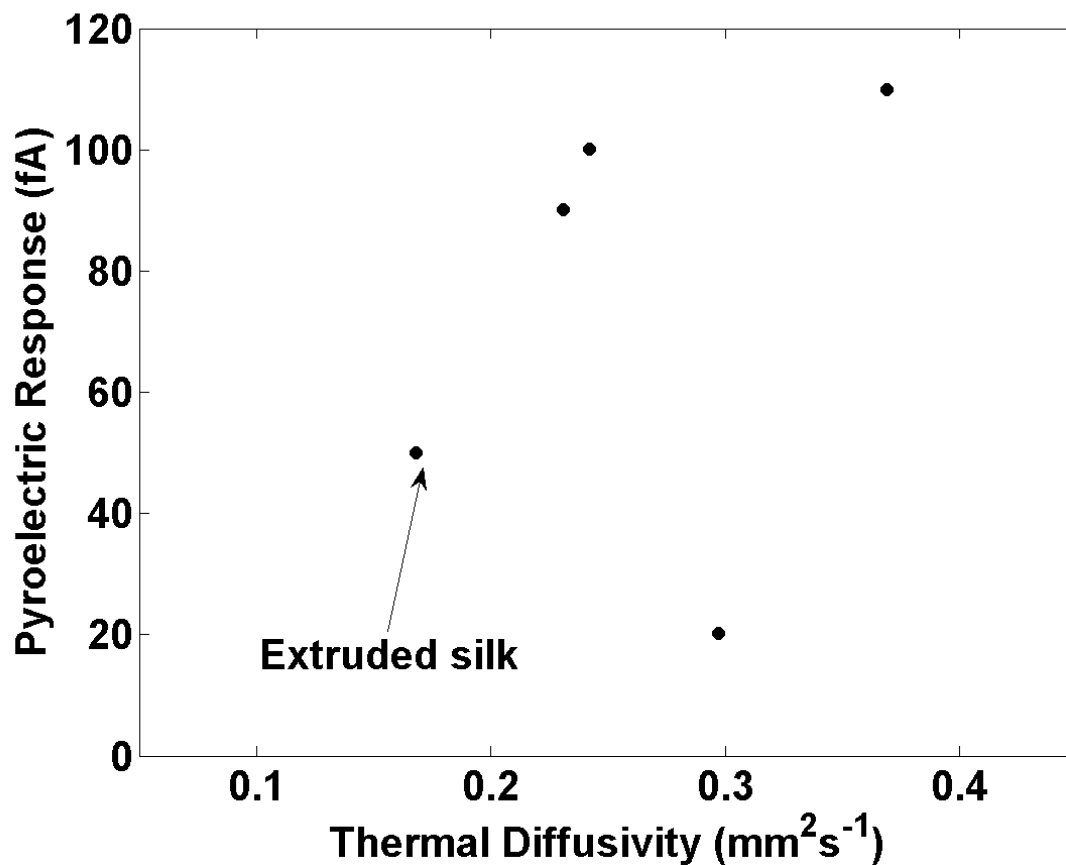


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5 **Figure 5.** SPEM dipole orientations of extruded synthetic silk fiber (top) compared to
6 processed synthetic silk fiber (bottom). Images on the left are at high frequencies and are
7 representative of behavior near the surface, while images on the right are at low frequencies
8 and are representative of behavior deeper inside the fiber.

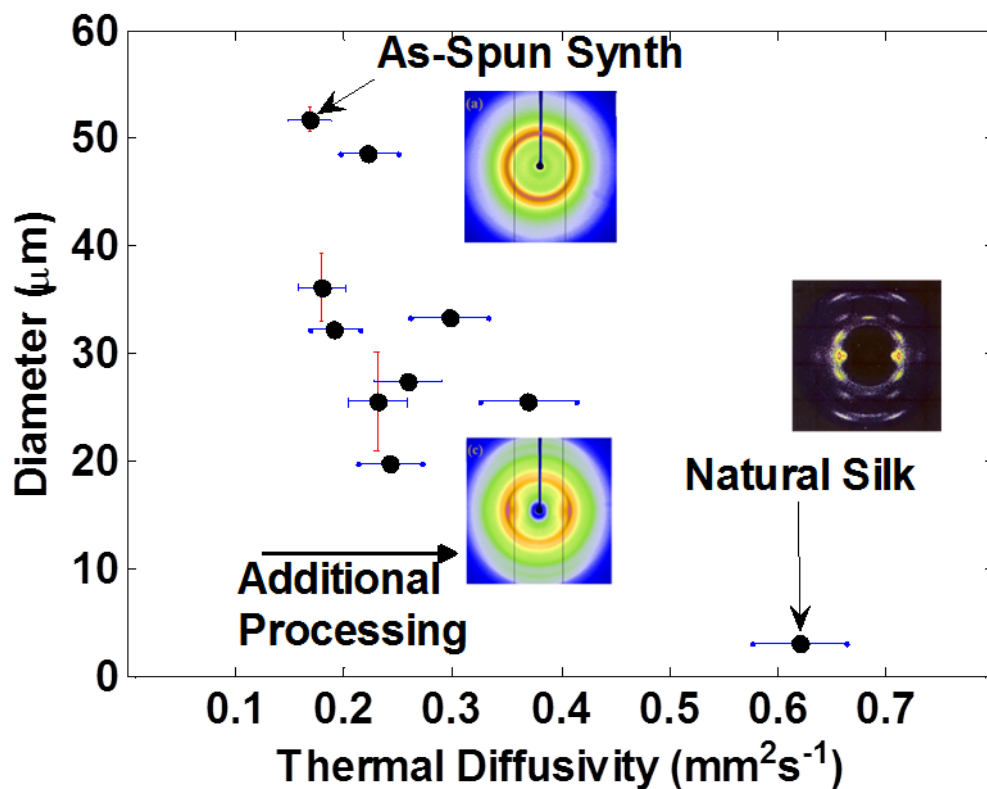
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3 **Figure 6.** Correlation between the thermal diffusivity and different mechanical properties,
4 measured in different processing conditions: ultimate tensile strength (top), maximum
5 extensibility (middle), and energy to break (bottom), showing the trend that processing of the
6 silk (via stretching and passing through water baths), improves both properties.



1
2 **Figure 7.** Pyroelectric current of spider silk compared to thermal diffusivity (based on laser
3 intensity modulated between 10-90 mW, and a sample reflectivity between 10-30%^[43]). The
4 presence and macroscopic alignment of crystalline sheets in the synthetic silk contribute to a
5 greater pyroelectric response, which is also mirrored in the thermal diffusivity.
6



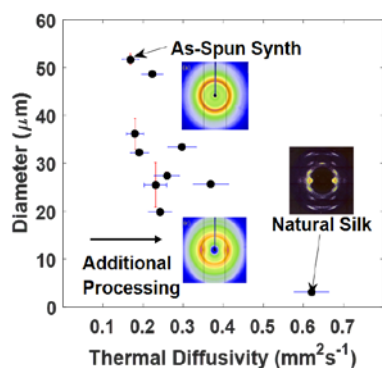
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 2 **Figure 8.** Thermal diffusivity of the natural dragline and synthetic spider silks, showing the
 3 trend to smaller diameters and improved thermal property as the fiber is put through
 4 additional processing treatments (multiple stretchings, multiple liquid baths). XRD diffraction
 5 patterns reprinted with permission from Refs.^[10,33], copyright 2015 and 1997 respectively.

1 **A correlation between the thermal properties, mechanical properties, pyroelectric**
2 **response, and diameter of natural and synthetic spider silk is observed for the first time.**
3 The results show that the processes during the synthetic fiber production induce crystal
4 formation and axial alignment, but the fibers still have different structural organization than
5 natural silks. (XRD diffraction patterns reprinted with permission from Refs.^[10,33], copyright
6 2015 and 1997 respectively).

7
8 **Keyword: spider silk, strength, toughness, thermophysical, pyroelectric**

9
10 T. Munro*, T. Putzeys, C. Copeland, C. Xing, R. Lewis, H. Ban, C. Glorieux, M.
11 Wubbenhorst

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13 **Title: Investigation of synthetic spider silk crystallinity and alignment via electrothermal,**
14 **pyroelectric, literature XRD, and tensile techniques**



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